



Brief Introduction to Radio Telescopes

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Terms and Concepts

Parabolic reflector
Blocked/unblocked
Subreflector
Frontend/backend
Feed horn
Local oscillator
Mixer
Noise Cal
Flux density

Jansky
Bandwidth
Resolution
Antenna power pattern
Half-power beamwidth
Side lobes
Beam solid angle
dB (deciBels)
Main beam efficiency
Effective aperture

Aperture efficiency
Antenna Temperature
Aperture illumination function
Spillover
Gain
System temperature
Receiver temperature
convolution





Text books on Radio Astronomy

- Essential Radio Astronomy
- https://science.nrao.edu/opportunities/courses/era

Essential Radio Astronomy



James J. Condon, Scott M. Ransom

Princeton University Press, Apr 5, 2016 - Science - 376 pages Essential Radio Astronomy is the only textbook on the subject specifically designed for a onesemester introductory course for advanced undergraduates or graduate students in More »

Search inside



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Tools of Radio Astronomy

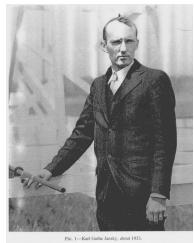
Authors: Wilson, Thomas, Rohlfs, Kristen, Huettemeister, Susanne

Presents the 6th edition of a leading textbook on radio astronomy to include state-of-the-art descriptions of instrumentation and new observations





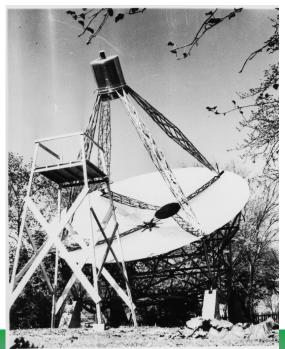
Pioneers of Radio Astronomy



Karl Jansky 1932



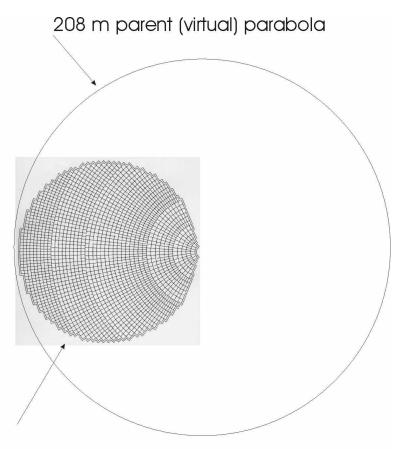


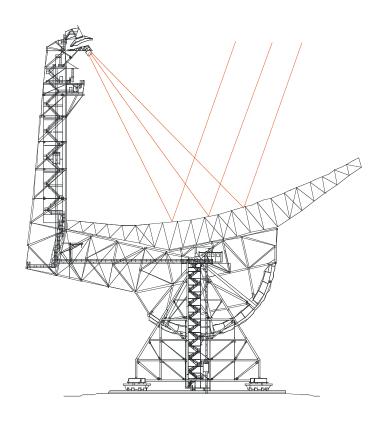




Unblocked Aperture

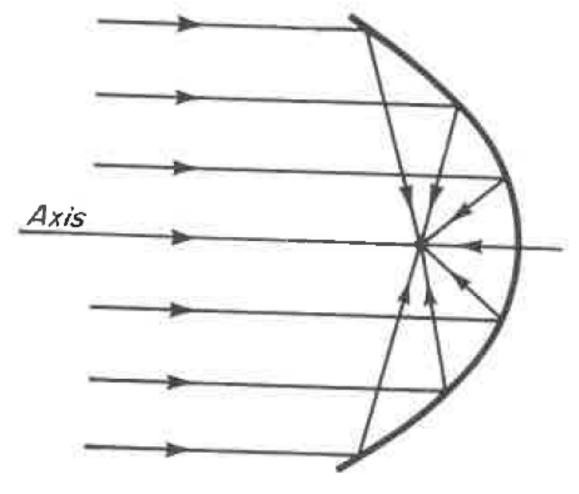
- 100 x 110 m section of a parent parabola 208 m in diameter
- Cantilevered feed arm is at focus of the parent parabola





GBT 100 x 110 m Parabola Section





Paraboloidal mirror









Subreflector and receiver room







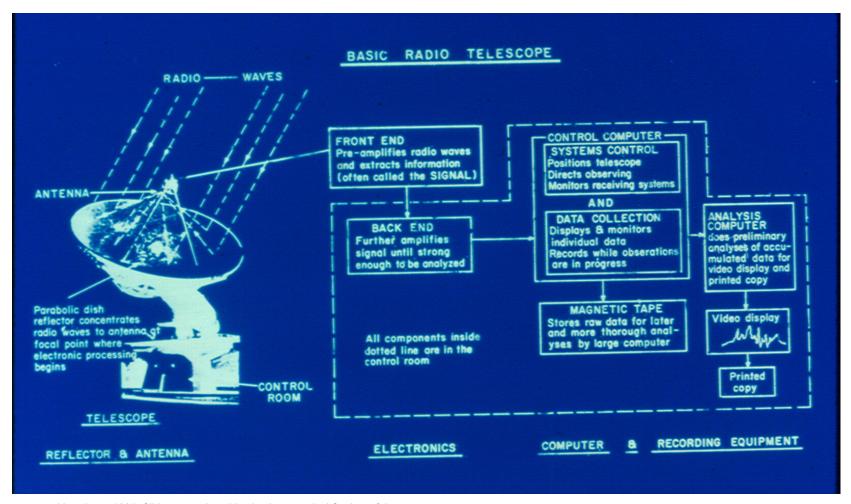
On the receiver turret





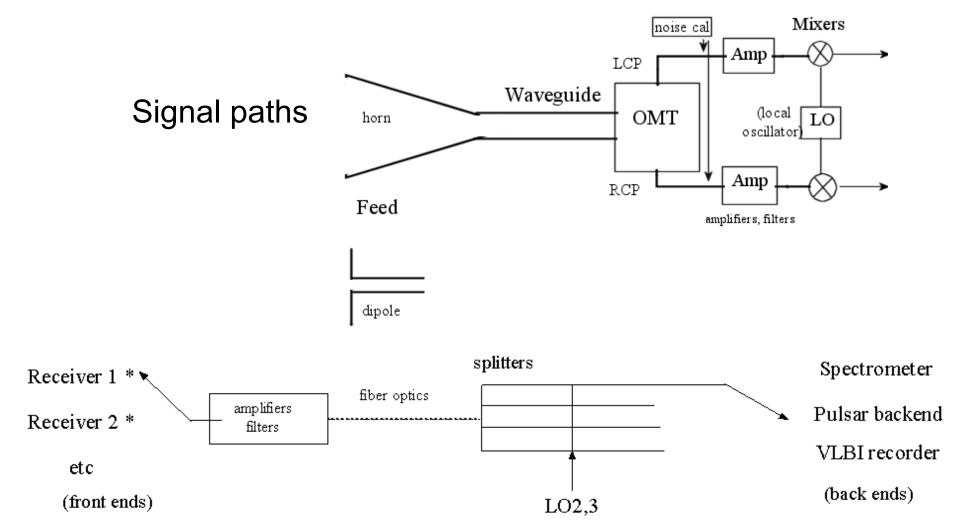


Basic Radio Telescopes



Verschuur, 1985. Slide set produced by the Astronomical Society of the Pacific, slide #1.







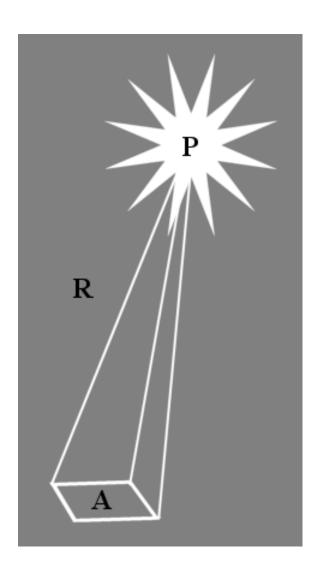
Intrinsic Power P (Watts)
Distance R (meters)
Aperture A (sq.m.)

Flux = Power/Area
Flux Density (S) =
Power/Area/bandwidth
Bandwidth (β)

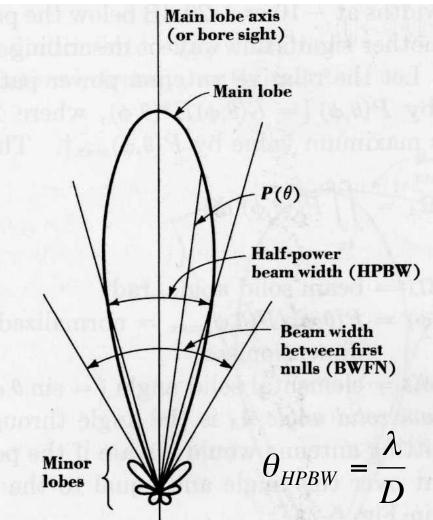
A "Jansky" is a unit of flux density

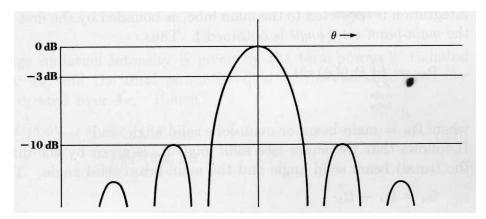
$$10^{-26}$$
 Watts / m^2 / Hz

$$P = 10^{-26} 4\pi R^2 S\beta$$



Antenna Beam Pattern (power pattern)





Beam Solid Angle (steradians)

$$\Omega_A = \iint_{A\pi} P_n(\theta, \phi) d\Omega$$

Main Beam Solid Angle

$$\Omega_{M} = \iint_{\substack{main\\lobe}} P_{n}(\theta, \phi) d\Omega$$

P_n = normalized power pattern





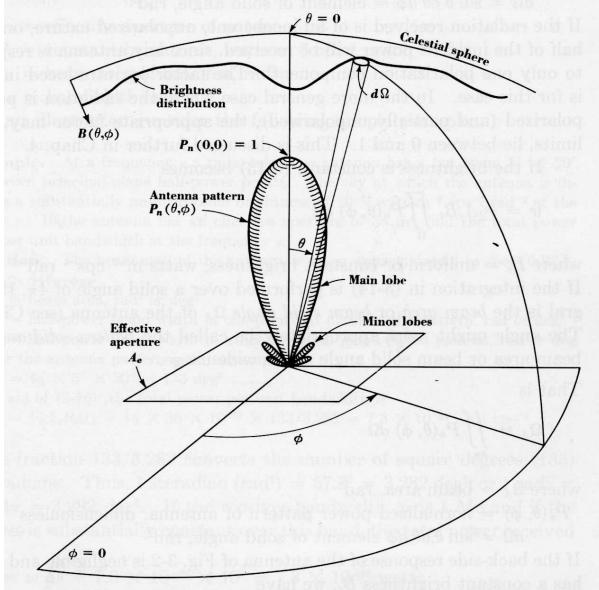


Fig. 3-2. Relation of antenna pattern to celestial sphere with associated coordinates.



dB ??

$$\Delta p(dB) = 10\log_{10}(\frac{P_1}{P_2})$$

P1/P2	$\Delta p(dB)$
1	0
2	3
10	10
100	20
1000	30





Convolution relation for observed brightness distribution

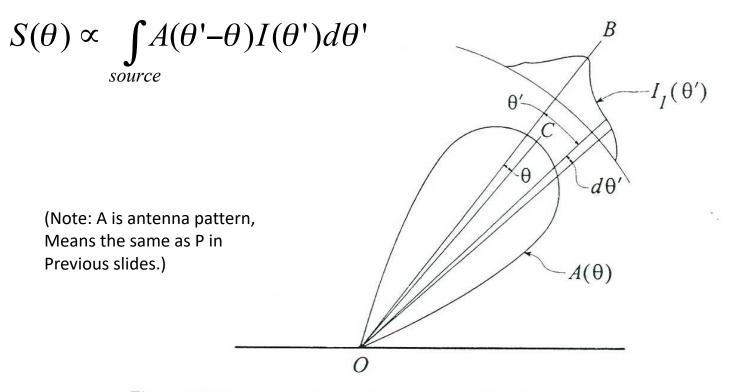


Figure 2.5 The power pattern of an antenna $A(\theta)$ and the intensity profile of a source $I_1(\theta')$ used to illustrate the convolution relationship. The angle θ is measured with respect to the beam center OC and θ' is measured with respect to the direction of the nominal position of the source OB.



Smoothing by the beam

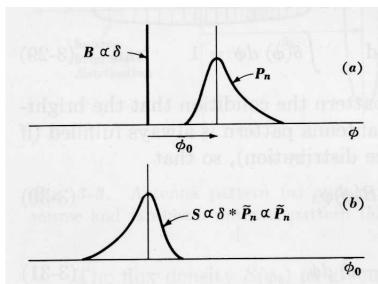


Fig. 3-6. For a point source the observed distribution is the same as the mirror image of the antenna pattern.

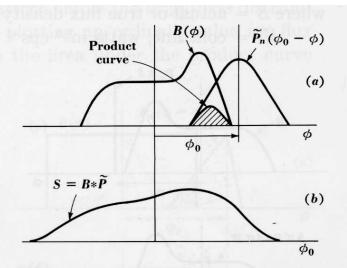


Fig. 3-4. The true brightness distribution B scanned by, or convolved with, the antenna pattern \tilde{P} , as in (a) yields the observed flux-density distribution S, as in (b).



Some definitions and relations

Main beam efficiency, ε_{M}

$$\varepsilon_{M} = \frac{\Omega_{M}}{\Omega_{A}}$$

Antenna theorem

$$\Omega_A = \frac{\lambda^2}{A_e}$$



Aperture efficiency, ε_{ap} Effective aperture, A_e Geometric aperture, A_a

$$\varepsilon_{ap} = \frac{A_e}{A_g}$$

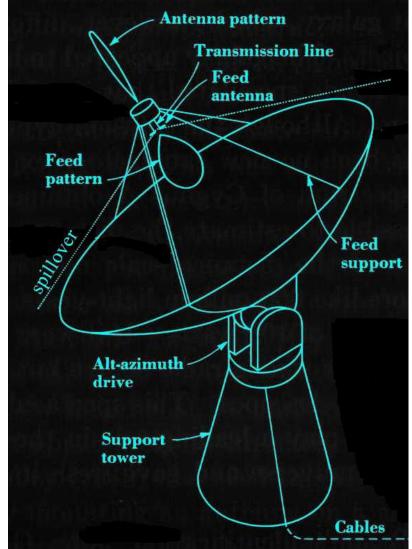
$$A_g(GBT) = \pi \left\{ \frac{1}{2} (100m) \right\}^2 = 7854m^2$$

$$\mathcal{E}_{ap} = \mathcal{E}_{pat} \mathcal{E}_{surf} \mathcal{E}_{block} \mathcal{E}_{ohmic} \cdots$$



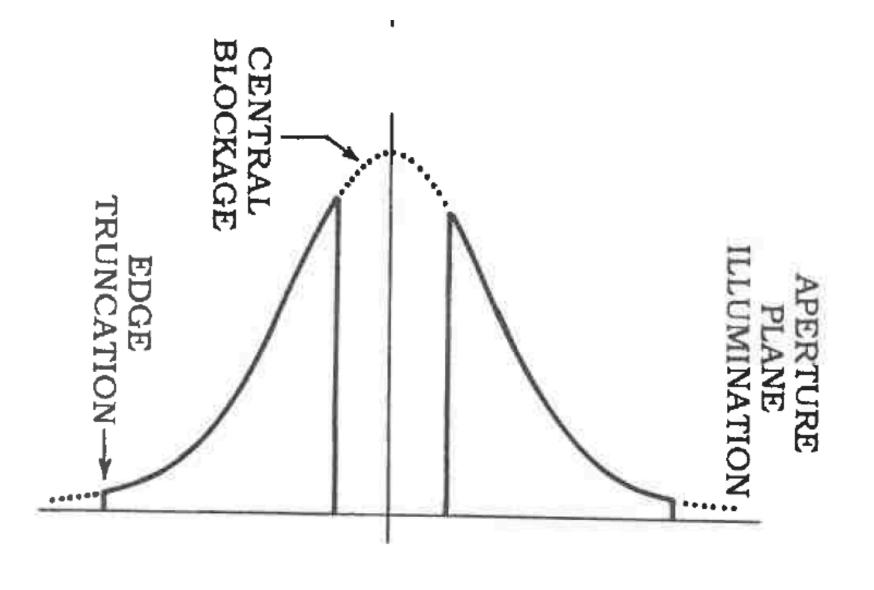


another Basic Radio Telescope



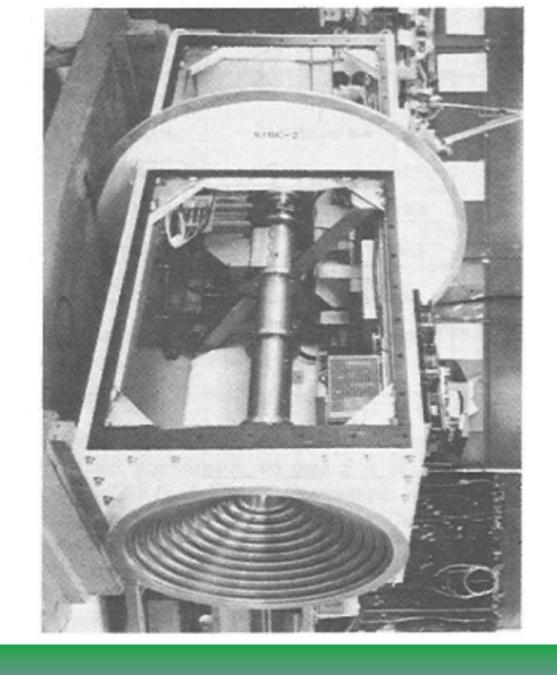












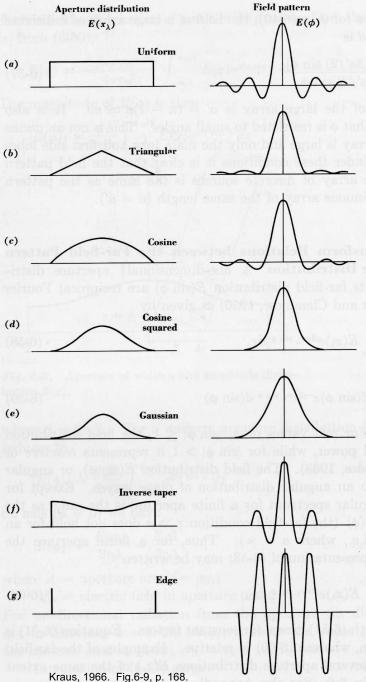




Aperture Illumination Function $\leftarrow \rightarrow$ Beam Pattern

A gaussian aperture illumination gives a gaussian beam:

$$\varepsilon_{pat} \approx 0.7$$







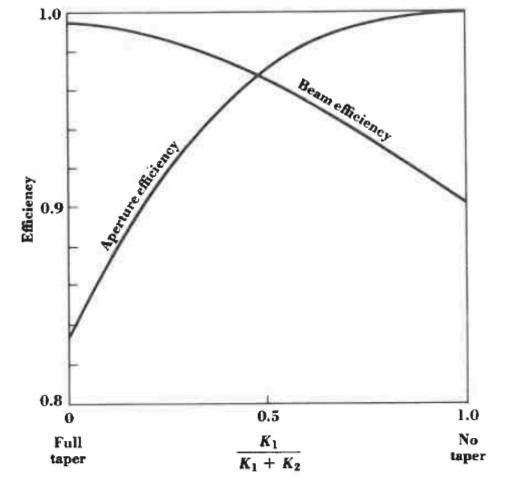
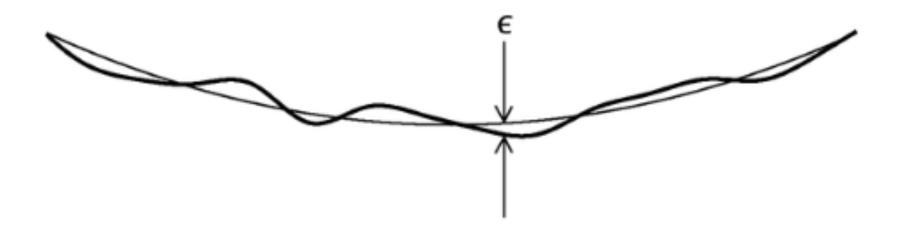


Fig. 6-104 Beam and aperture efficiencies for a one-dimensional aperture as a function of taper. (After Nash, 1964.) The aperture efficiency is a maximum with no taper, while the beam efficiency is a maximum with full taper.





Not-quite-perfect parabola

 σ = rms surface error





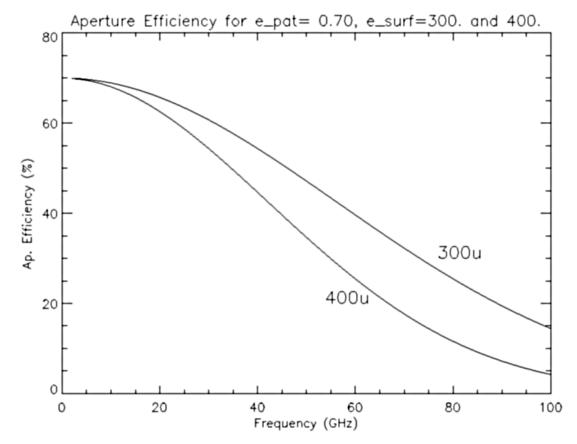
Surface efficiency -- Ruze formula

$$\varepsilon_{surf} = e^{-(4\pi\sigma/\lambda)^2}$$

 σ = rms surface error

Effect of surface efficiency

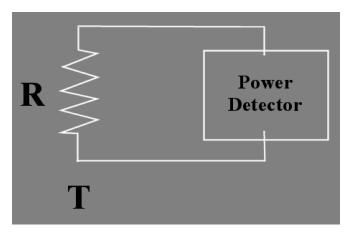
$$\varepsilon_{ap} = \varepsilon_{pat} \varepsilon_{surf} \cdots$$



John Ruze of MIT -- Proc. IEEE vol 54, no. 4, p.633, April 1966.



Detected power (P, watts) from a resistor R at temperature T (kelvin) over bandwidth $\beta(Hz)$



$$P = kT\beta$$

Power P_A detected in a radio telescope Due to a source of flux density S

$$P_A = \frac{1}{2} A S \beta$$

power as equivalent temperature.

Antenna Temperature T_A Effective Aperture A_e

$$S = \frac{2kT_A}{A_e}$$



System Temperature

= total noise power detected, a result of many contributions

$$T_{sys} = T_{ant} + T_{rcvr} + T_{atm} (1 - e^{-\tau a}) + T_{spill} + T_{CMB} + \cdots$$

Thermal noise ΔT

= minimum detectable signal

$$\Delta T = k_1 \frac{T_{sys}}{\sqrt{\Delta v \cdot t_{int}}}$$

The Radiometer Equation

Gain(K/Jy) for the GBT

$$S = \frac{2kT_A}{A_e}$$

Including atmospheric absorption:

$$S = \frac{2kT_A}{A_e}e^{\tau a}$$

$$G = \frac{T_A}{S} = \frac{\varepsilon_{ap} A_g}{2k}$$

$$G(K/Jy) = 2.84 \cdot \varepsilon_{ap}$$

Physical temperature vs antenna temperature

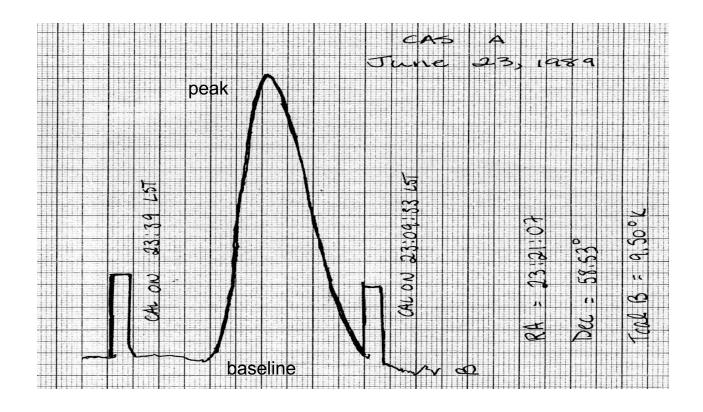
For an extended object with source solid angle Ω_s , And physical temperature T_s , then

for
$$\Omega_s < \Omega_A$$
 $T_A = \frac{\Omega_s}{\Omega_A} T_s$

for
$$\Omega_s > \Omega_A$$
 $T_A = T_s$

In general :
$$T_A = \frac{1}{\Omega_A} \iint_{source} P_n(\theta, \phi) T_s(\theta, \phi) d\Omega$$

Calibration: Scan of Cass A with the 40-Foot



Tant = Tcal * (peak-baseline)/(cal – baseline)

(Tcal is known)

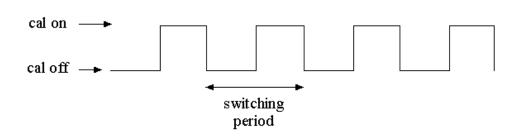




More Calibration: GBT

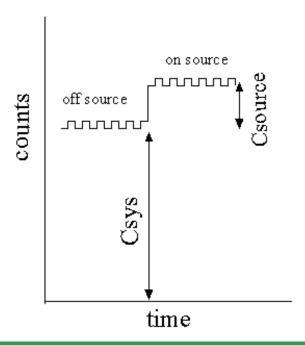
Convert counts to T

$$K = \frac{T_{cal}}{\left\langle C_{cal-on} - C_{cal-off} \right\rangle}$$



$$\begin{split} T_{sys} &= K \cdot C_{sys} \\ &= \frac{1}{2} K \cdot (C_{offsource, calon} + C_{offsource, caloff}) - \frac{1}{2} T_{cal} \end{split}$$

$$T_{ant} = K \cdot C_{source}$$



Scan 182 0.0 RADI-LSR FO : 1.42041 GHz Pol: YY 2009-05-29 Int : 00 00 54.3 Fsky: 1.41836 GHz IF: 0 Katie Chynoweth LST: +05 24 59.4 BW : 12.5000 MHz AGBT09B_034_01 OnOff 07 36 51.38 +65 36 09.4 Az: 384.4 El: 56.9 HA: -2.20 Position switching V : 0.0 RADI-LSR F0 : 1.42041 GHz Pol: YY Int : 00 00 27.2 Fsky : 1.41836 GHz IF : 0 Scan 182 Tsys: 17.27 2009-05-29 Katie Chynoweth LST: +05 24 59.4 BW : 12.5000 MHz AGBT09B_034_01 OnOff 07 36 51.38 +65 36 09.4 Az: 384.4 El: 56.9 HA: -2.20 1.416 1.418 1.420 1.414 TOPO Frequency (GHz) bdrop: 40 edrop: 0 Scan 183 2009-05-29 Katie Chynoweth 07 46 29.30 +66 36 01.9 1.414 1.416 1.418 1.420 1.422 1.424 TOPO Frequency (GHz) bdrop: 40 edrop: 0 Sun Jul 12 11:36:39 2009 GREEN BANK 1.414 1.416 1.418 1.420 1.422 1.424 TOPO Frequency (GHz) bdrop: 40 edrop: 0 Sun Jul 12 11:35:51 2009



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